



# ENM061 - Power Electronic Converters

## 7.5 ECTS, 2017

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## Lecture outline

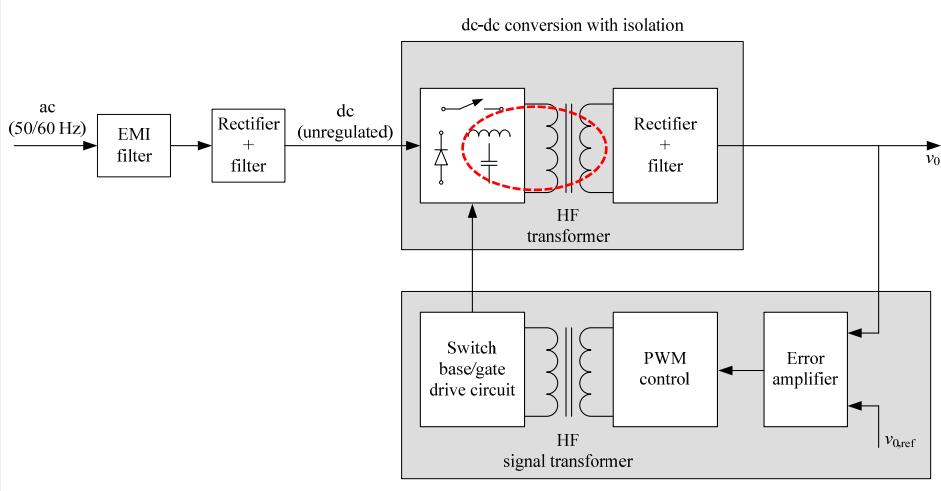
### **Passive components**

- Resistors
- Capacitors
- Inductors
- Magnetic circuits and analogy to electrical circuits
- Transformers
- Brief description of the Tutorial and PSpice exercises
- Summary

## Learning outcomes

- Fourier components and total harmonic distortion (THD) for basic waveforms.
- Operating principles of the most common active components (e.g. diode, thyristor, IGBT, and MOSFET) and passive components (e.g. capacitors, transformers and inductors).
- Operation of a pulse width modulation (PWM), the purpose of controlling the desired quantity and the need for a controller circuit within the power electronic converter.
- Analysis of ideal DC/DC converters (e.g. buck, boost, buck-boost, flyback, the forward, the push-pull, half-bridge and full-bridge converters) in CCM and DCM operation.
- Operating principles of single-phase and three-phase AC/DC inverters with different modulation strategies (e.g. PWM and square wave operation).
- Operation of multilevel converters (e.g. NPC, flying capacitor and MMC topologies) using current and voltage waveform analysis. Pros and Cons of the converter in terms of harmonics and losses.
- Operation of single- and three-phase diode rectifiers operating with voltage-stiff and current-stiff DC-side. Investigating the impact of line impedance within the converter circuit for current commutation.
- Operation of single- and three-phase thyristor rectifiers operating with a current-stiff DC-side and the impact of line impedance for current commutation. Investigating the use of 6/12-pulse configurations.
- Identify simple power electronic converter schematics. Recognizing the different parts in a physical circuit on which basic wave-shape and efficiency measurements is performed.
- Loss calculation in passive and active components. Evaluating the temperature rise in the active components and choosing an appropriate heat-sink. Gaining a basic understanding of component life time.
- Utilizing the software Cadence PSpice to simulate basic power electronic circuits and the practical labs to have a firsthand experience of how real DC/DC converters operate.

## Switch-mode power supply



Undeland, Power Electronics  
Figure 10 - 2, page 303

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## Switch-mode power supply

### Equivalent circuit

**Average load voltage**

$$V_0 = \frac{1}{T_s} \int_0^{T_s} v_{oi} dt = \frac{t_{on}}{T_s} V_d = DV_d$$

**Switching function**

$$\text{switch } a = \begin{cases} \text{on} \Rightarrow \text{Diode off}, V_{0,\text{ref}} \geq V_{tri} \\ \text{off} \Rightarrow \text{Diode on}, V_{0,\text{ref}} < V_{tri} \end{cases}$$

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## Resistors – Non Ideal Circuit Models

- Parasitic effects must be accounted for in high frequency applications

- Ideal model

$$R = \frac{\rho l}{A}$$

- Non-ideal model

- Various loads and losses are usually represented by an equivalent resistance

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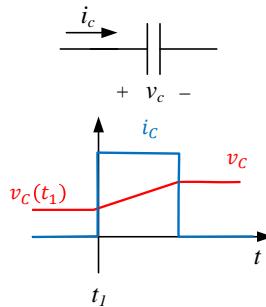
## Capacitors – Ideal Behavior

$$i_c = C \frac{dv_c}{dt}$$

Average and RMS current and voltage?

$$v_c = v_c(t_1) + \frac{1}{C} \int i_c dt$$

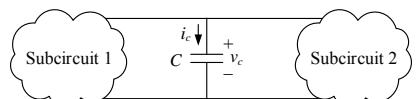
Voltage stiff component



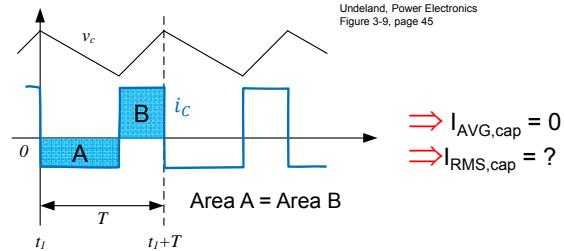
## Capacitors – Ideal Behavior

The current-time areas (charge) are equal – no net storage of charges

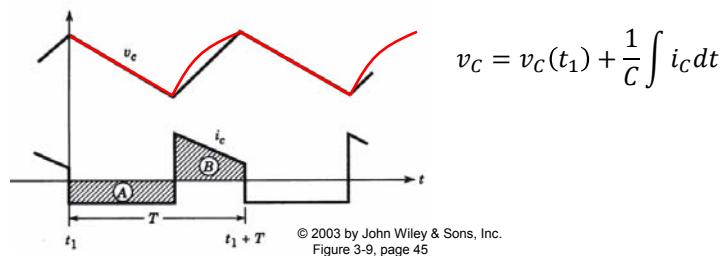
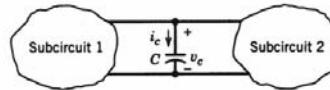
$$v_c = v_c(t_1) + \frac{1}{C} \int i_c dt$$



Udeland, Power Electronics  
Figure 3-9, page 45



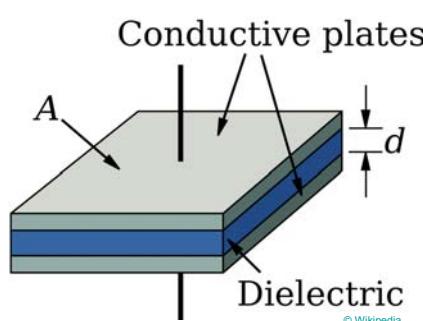
## Capacitors – Ideal Behavior



Ex.: what is wrong in this figure?

## Capacitors – Physical Design

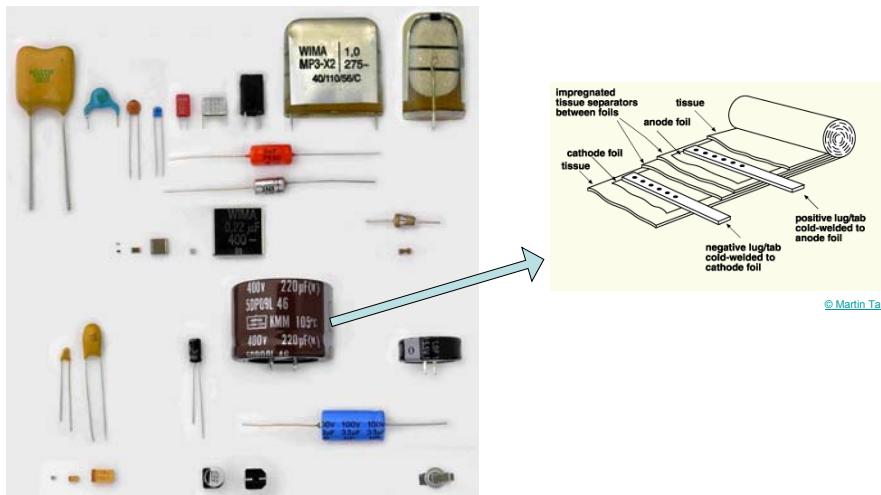
The capacitance is determined by  $C = \frac{\epsilon A}{d}$



- The larger the plate area, the larger the capacitance value
- The smaller distance between the plates, the larger capacitance value
- The larger dielectric constant, the larger the capacitance

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## Capacitors – Physical Design



The collage includes several physical capacitors of different sizes and colors (yellow, blue, red, black), some with visible markings like 'WIMA 1.0 MF3-X2 275-40/11056/C' and 'WIMA 0.22 µF 400V'. To the right is a detailed cross-section diagram of a capacitor cell. The diagram shows a stack of alternating layers: anode foil, tissue, and cathode foil, with 'impregnated tissue separators between foils'. It also shows 'tissue' and 'cathode foil' layers. Two 'lug/tabs' are shown, one 'positive lug/tab cold-welded to anode foil' and one 'negative lug/tab cold-welded to cathode foil'. A blue arrow points from the text 'positive lug/tab cold-welded to anode foil' to the positive lug/tab in the diagram. The source is cited as '© Martin Tarc'.

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## Capacitors for Power Systems

Capacitor Banks – Applications		
Flexible AC Transmission Systems (FACTS)	Parallel Compensation	Static Var Compensator (SVC)
		Mechanically Switched Capacitor with Damping Network (MSCDN)
Series Compensation		Mechanically Switched Capacitors (MSC)
		Thyristor Controlled Series Compensation (TCSC)
		Thyristor Protected Series Compensation (TPSC)
	Fixed Series Compensation (FSC)	

AC Harmonic Filters  
AC PLC Filters  
Long Distance and Back-to-Back HVDC – AC & DC Filters  
AC & DC Surge Capacitors

© Siemens

Technical data	
Type	impregnated all-film dielectric
Rated voltage	up to 8 kV
Rated frequency	50 Hz or 60 Hz
Rated power	up to 850 kvar
Average losses	< 0.15 W/kvar
Dielectric liquid	non-pcb
All-film dielectric	polypropylene
Temperature category	-50° C to +55° C (0)
Standards	IEC 60871-1 ANSI/IEEE, CSA
Standard colour	Light grey (RAL 7035)



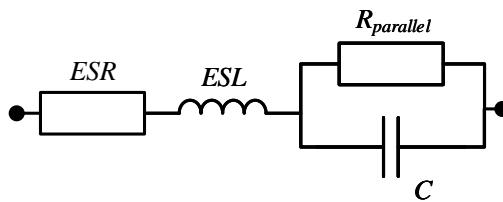
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# Capacitors – Non-Ideal Circuit Models

Simple capacitor model that accounts for:

- The insulation resistance (if necessary)
- The equivalent series inductance (if necessary)
- The equivalent series resistance (ESR)



# Capacitors – Non-Ideal Behavior

Type ⊕ = polarized	Pic	Cap Range	ESR	Leakage	Voltage Rating	Temp Range	Gen Notes
Ceramic		pF - $\mu$ F	low	med	high	-55° to +125°C	Multipurpose Cheap
Mica (silver mica)		pF - nF	low 0.01-0.1Ω	low	high	-55° to +125°C	For RF filters Expensive Very stable
Plastic Film (polyethylene polystyrene)		few $\mu$ Fs	med	med	high	varies	For low freq Cheap
Tantalum		$\mu$ Fs	high 0.5-5.0Ω	low	lowest	-55° to +125°C	Expensive Nonlinear (bad for audio)
OSCON		$\mu$ Fs	low 0.01-0.5Ω	low	low	-55° to +105°C	Best quality Highest price
Aluminum Electrolytic		high $\mu$ Fs	high 0.05-2.0Ω	med	low	-40° to +85°C	For low-med frequencies Cheap Hold charge for long time – not for production test



## Capacitors – Non-Ideal Behavior

- **Leakage current and insulation resistance**

A small DC-current will flow through the dielectric due to non-idealities.  
Temperature and material dependent.

- **Dielectric strength**

Breakdown of the dielectric material due to high electric fields.  
Usually leads to a short circuit of the capacitor

- **Equivalent series resistance (ESR)**

The sum of all ohmic losses and dielectric losses within the capacitor. It depends on material, temperature and frequency. It decides rated RMS-current due to internal heating.

- **Dissipation factor ( $\tan \delta = \text{ESR}/|X_c|$ )**

The ratio of the resistive power loss in ESR to the reactive power oscillating in the capacitor. It is the inverse of Q-factor.

i.e.,  $Q_f = \omega^2 \text{maximum stored energy}/\text{dissipated power}$



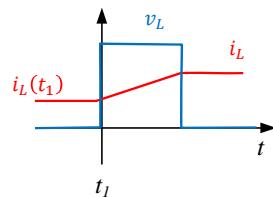
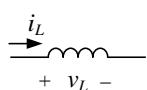
## Inductors

$$v_L = L \frac{di_L}{dt}$$

Average and RMS current and voltage?

$$i_L = i_L(t_1) + \frac{1}{L} \int v_L dt$$

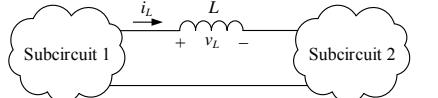
Current stiff component



# Inductors

The volt-second areas are equal – no net storage of magnetic energy

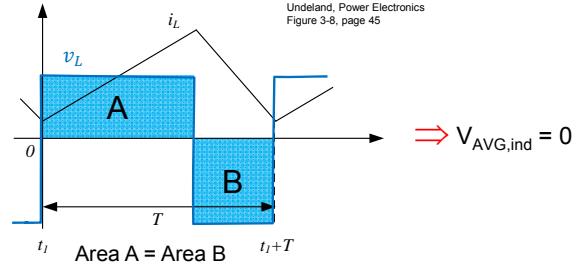
$$i_L = i_L(t_1) + \frac{1}{L} \int v_L dt$$



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Figure 3-8, page 45

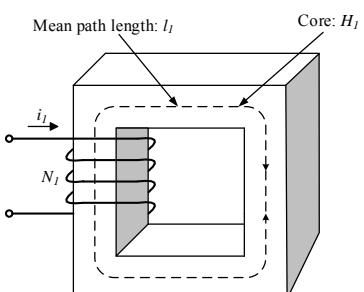
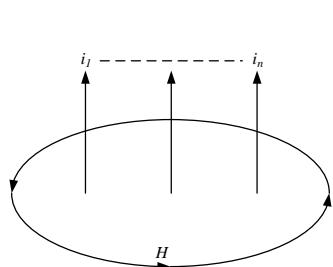
Ex.: *Plot the waveform of  $v_L$*



# Inductors

## Ampere's Law and the H-Field

Any current carrying unit produces a magnetic field of intensity  $H$  (A/m).



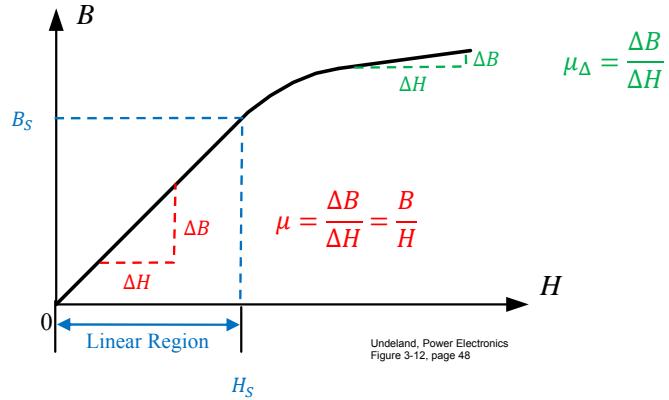
$$\oint H dl = \sum i$$

$$\sum_k H_k l_k = \sum_m N_m i_m$$

# Inductors

## The Relationship Between B and H

$$B = \mu H = \mu_r \mu_0 H$$

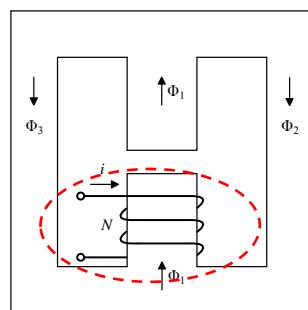


# Inductors

## Flux and Analogy to Electric Circuits

$$\Phi = \iint_A B \, dA$$

The B-field (flux density) over an area gives the total flux. Magnetic flux lines form closed loops (continuity of flux) and an analogy can be made to electric current and voltage

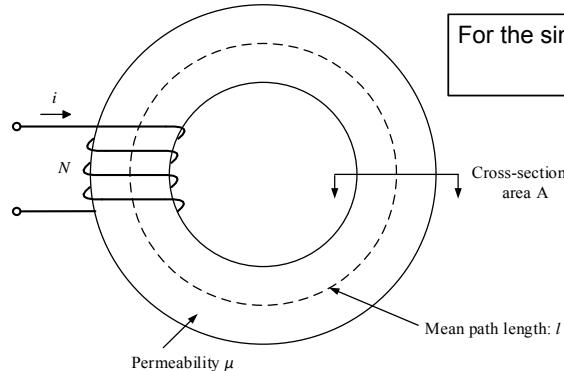


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Figure 3-15, page 51

# Inductors

## Magnetic Resistance

$$\sum_k H_k l_k = \sum_m N_m i_m \rightarrow \Phi \sum_k \frac{l_k}{\mu_k A_k} = \sum_m N_m i_m \quad \mathfrak{R}_k = \frac{l_k}{\mu_k A_k}$$



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 Figure 3-14, page 49

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# Inductors

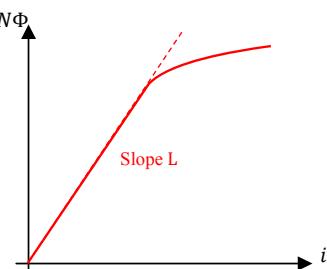
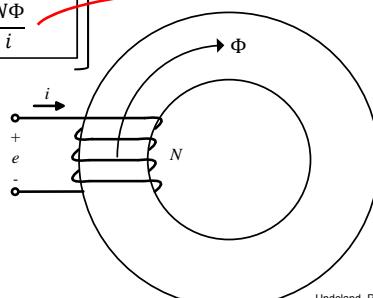
## Inductance Definition

Faraday's Law:  
 $e = N \frac{d\Phi}{dt}$

Definition of Inductance:  
 $L = \frac{N\Phi}{i}$

$$e = L \frac{di}{dt} + i \frac{dL}{dt} = L \frac{di}{dt}$$

From  $\Phi \mathfrak{R} = Ni \rightarrow$   
 $L = \frac{N N i}{i \mathfrak{R}} = \frac{N^2}{\mathfrak{R}}$



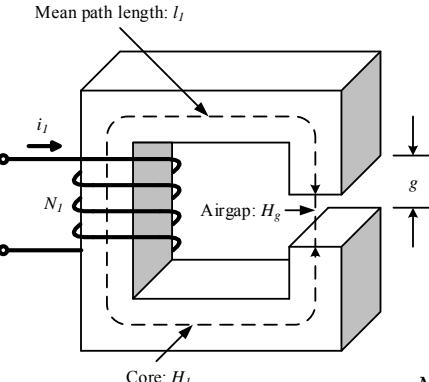
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 Figure 3-17, page 52

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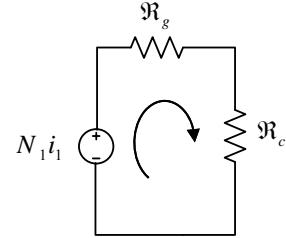
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# Inductors

## The Effect of an Airgap



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Figure 3-10, page 46



$$N_l i_l = \Phi (\mathfrak{R}_g + \mathfrak{R}_c)$$

$$\mathfrak{R}_c = \frac{l_c}{\mu_r \mu_0 A_c} [H^{-1}]$$

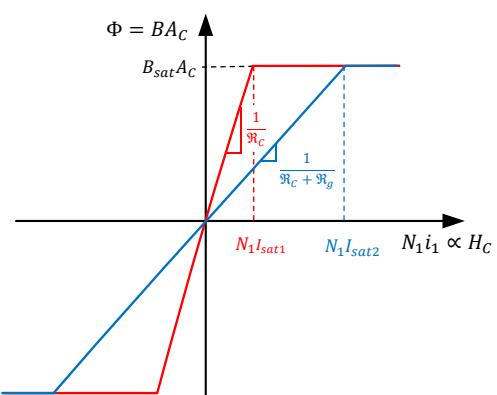
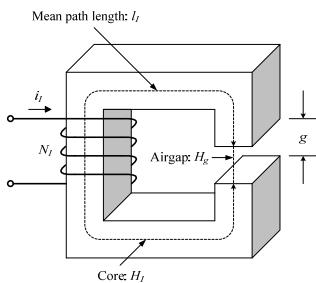
$$\mathfrak{R}_g = \frac{l_g}{\mu_0 A_c} [H^{-1}]$$

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# Inductors

## The Effect of an Airgap



$$N_l i_l = \Phi (\mathfrak{R}_g + \mathfrak{R}_c)$$

$$L = \frac{N_l^2}{\mathfrak{R}_g + \mathfrak{R}_c}$$

$$\Phi_{sat} = B_{sat} A_c$$

$$I_{sat} = \frac{B_{sat} A_c}{N_l} (\mathfrak{R}_g + \mathfrak{R}_c)$$

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# Inductors

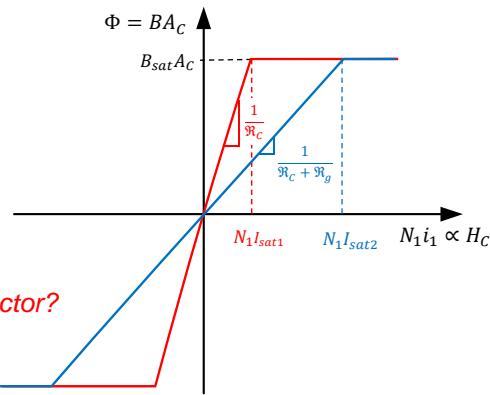
## The Effect of an Airgap

- No airgap – the inductance is determined by the core

$$L_1 = \frac{N_1^2}{\mathfrak{R}_c}$$

- With airgap – the inductance is determined by the airgap

$$L_2 = \frac{N_1^2}{\mathfrak{R}_g + \mathfrak{R}_c}$$



Ex.: *do we need an air-gap in an inductor?*

$$\frac{1}{2} L_1 I_{sat1}^2 < \frac{1}{2} L_2 I_{sat2}^2$$

$$\Downarrow \quad \Downarrow$$

$$\frac{1}{2} B_{sat} A_C N_1 I_{sat1} < \frac{1}{2} B_{sat} A_C N_1 I_{sat2}$$

# Inductors

## Core Materials

Core type	$B_{sat}$	Relative core loss	Applications
Laminations iron, silicon steel	1.5 - 2.0 T	high	50-60 Hz transformers, inductors
Powdered cores powdered iron, molypermalloy	0.6 - 0.8 T	medium	1 kHz transformers, 100 kHz filter inductors
Ferrite Manganese-zinc, Nickel-zinc	0.25 - 0.5 T	low	20 kHz - 1 MHz transformers, ac inductors

# Inductors

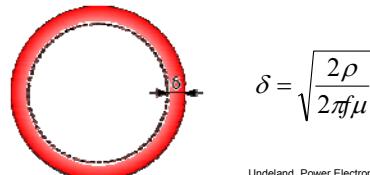
## Copper Losses

- DC resistance of wire

$$R = \rho \frac{l_b}{A_w}$$

where  $A_w$  is the wire bare cross-sectional area, and  $l_b$  is the length of the wire. The resistivity  $\rho$  is equal to  $1.724 \cdot 10^{-6} \Omega \text{ cm}$  for soft-annealed copper at room temperature. This resistivity increases to  $2.3 \cdot 10^{-6} \Omega \text{ cm}$  at  $100^\circ\text{C}$ .

- Skin effect – the current crowds at the edges of a conductor due to eddy currents within the material



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Chapter 30-1-3 and 30-2-3

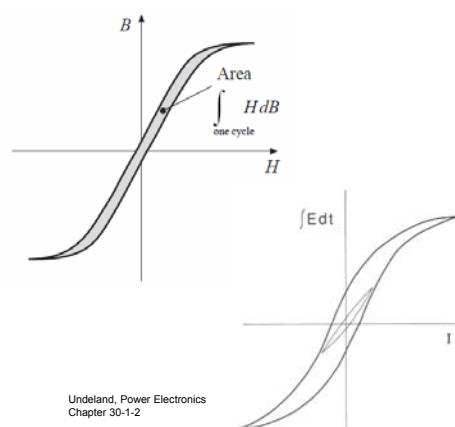
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# Inductors

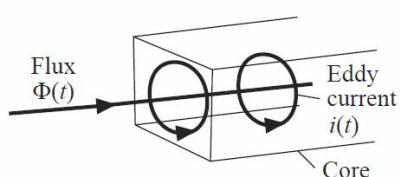
## Core Losses

- Hysteresis losses



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- Eddy current losses



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Chapter 30-1-4

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# Inductors

## Different Core Types

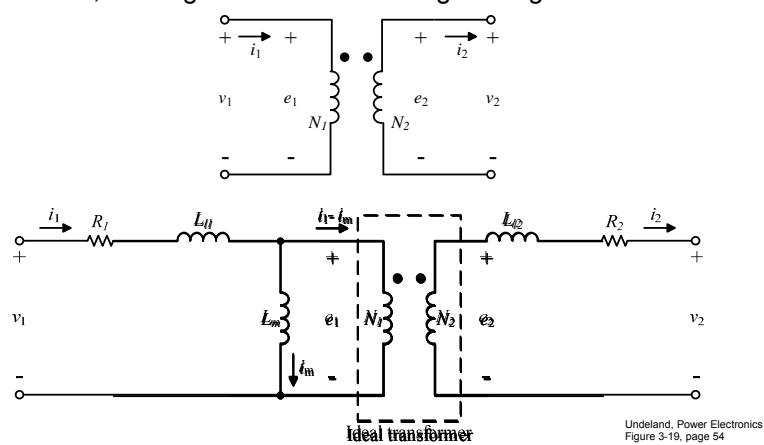


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# Transformers

- The equivalent circuit of the transformer including leakage inductances, winding resistances and magnetizing inductance.

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Figure 3-19, page 54

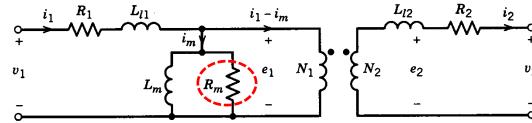
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Lecture 3 – 29/36

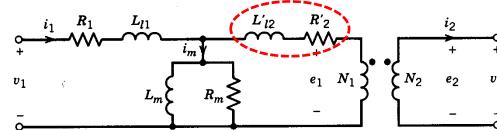
# Transformers

- The equivalent circuit of the transformer including leakage inductances, winding resistances and magnetizing inductance.

Including core losses

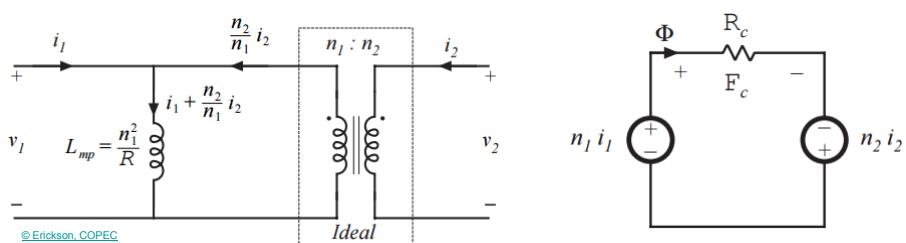


referring the components to the primary side



Undeland, Power Electronics  
Figure 3-21, page 56

# Transformers



For nonzero core reluctance, we obtain

$$\Phi R = n_1 i_1 + n_2 i_2 \quad \text{with} \quad v_1 = n_1 \frac{d\Phi}{dt}$$

Eliminate  $\Phi$ :

$$v_1 = \frac{n_1^2}{R} \frac{d}{dt} \left[ i_1 + \frac{n_2}{n_1} i_2 \right] \quad \text{Ex.: Derive } L_{mp}$$

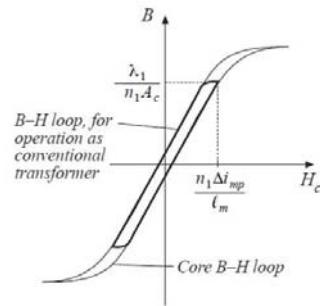
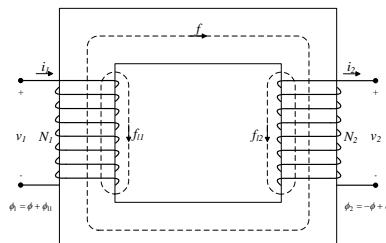
This equation is of the form

$$v_1 = L_{mp} \frac{di_{mp}}{dt}$$

$$\text{with} \quad L_{mp} = \frac{n_1^2}{R} \quad i_{mp} = i_1 + \frac{n_2}{n_1} i_2$$

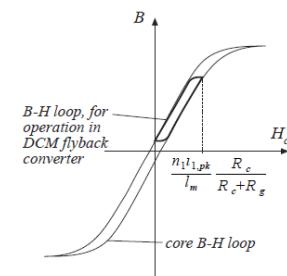
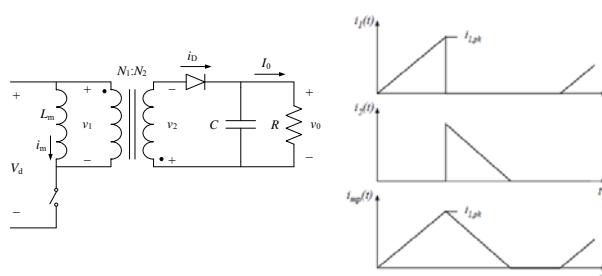
# AC Transformer

- Core losses, copper losses and proximity losses are usually significant.
- No air gap in the core.
- The core is usually made of laminated steel.

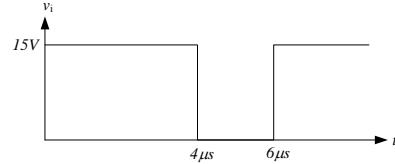
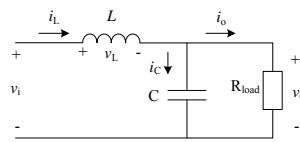


# Switched Converter Transformer

- Core losses, copper losses and proximity losses are usually significant.
- An air gap could be introduced to avoid saturation (eg. Flyback)
- The core is made of ferrite due to the high switching frequency.



## Tutorial 2

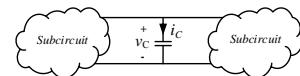
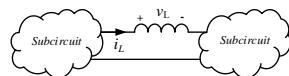


$V_i$  repetitive and system in steady state.  $L = 5\mu H$ ,  $C = \text{large}$ ,  $P_{\text{load}} = 250W$

- Average load voltage, average load current, capacitor RMS-current?
- What is the function of L and C?

## PSpice 1

Power electronic circuits and Fourier analysis in Cadence PSpice



- Waveforms for different inputs
- Steady-state operation?
- Waveforms for different inputs
- Steady-state operation



## Summary

- Explain the voltage and current relationship for an inductor and a capacitor and explain what it means.
- What does ESR represent in a transformer.
- What do copper losses and core losses represent in an inductor and a transformer?
- What is the electrical analogy for a flux and reluctance in a magnetic circuit?
- Can you motivate why we use an air-gap in an inductor?
- Can you sketch the equivalent circuit representation of an ideal and non-ideal transformer?
- Learning outcome:
  - ❖ Operating principles of the most common passive components (e.g. capacitors, transformers and inductors).